



# Realistic modeling for Security Constrained AC Optimal Power Flow (SC-ACOPF)

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Patrick Panciatici  
Scientific Advisor

**Rte**

Réseau de transport d'électricité

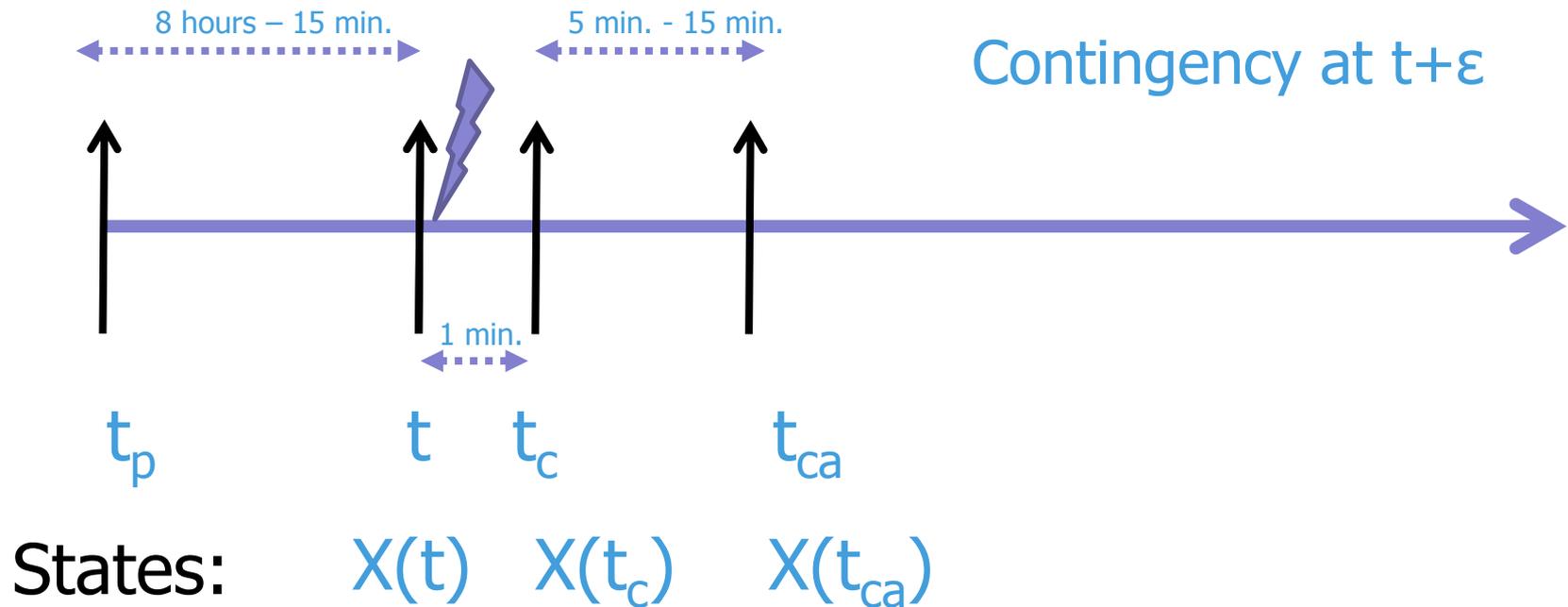
# OUTLINE

- **Why realistic modeling for SC-ACOPF?**
- **SC-ACOPF → multi stage process**
- **Closed loop controls in static modeling**
  
- **Some modeling issues**
  
- **Overview of 3 examples:**
  - Synchronous generators
  - HVDC links: LCC & VSC
  - Active Distribution Networks
  
- **Data format et data availability?**

# Why realistic modeling for SC-ACOPF?

- ▶ Find “optimal” decisions for system operation, market operation, grid maintenance and grid expansion.
- ▶ Definition of an acceptable risk is a prerequisite and security constrained AC OPF is mandatory.
  - In stressed conditions, optimizations based on DC approximation fail, exactly when tool should be helpful in decision making process.
- ▶ Need for realistic modeling for reactive/voltage behaviors and corrective actions
- ▶ Not only for actual systems but also for future possible evolutions: we must evaluate benefits of technological options before their implementations!

# SC-ACOPF Multi stage process (Static modeling)

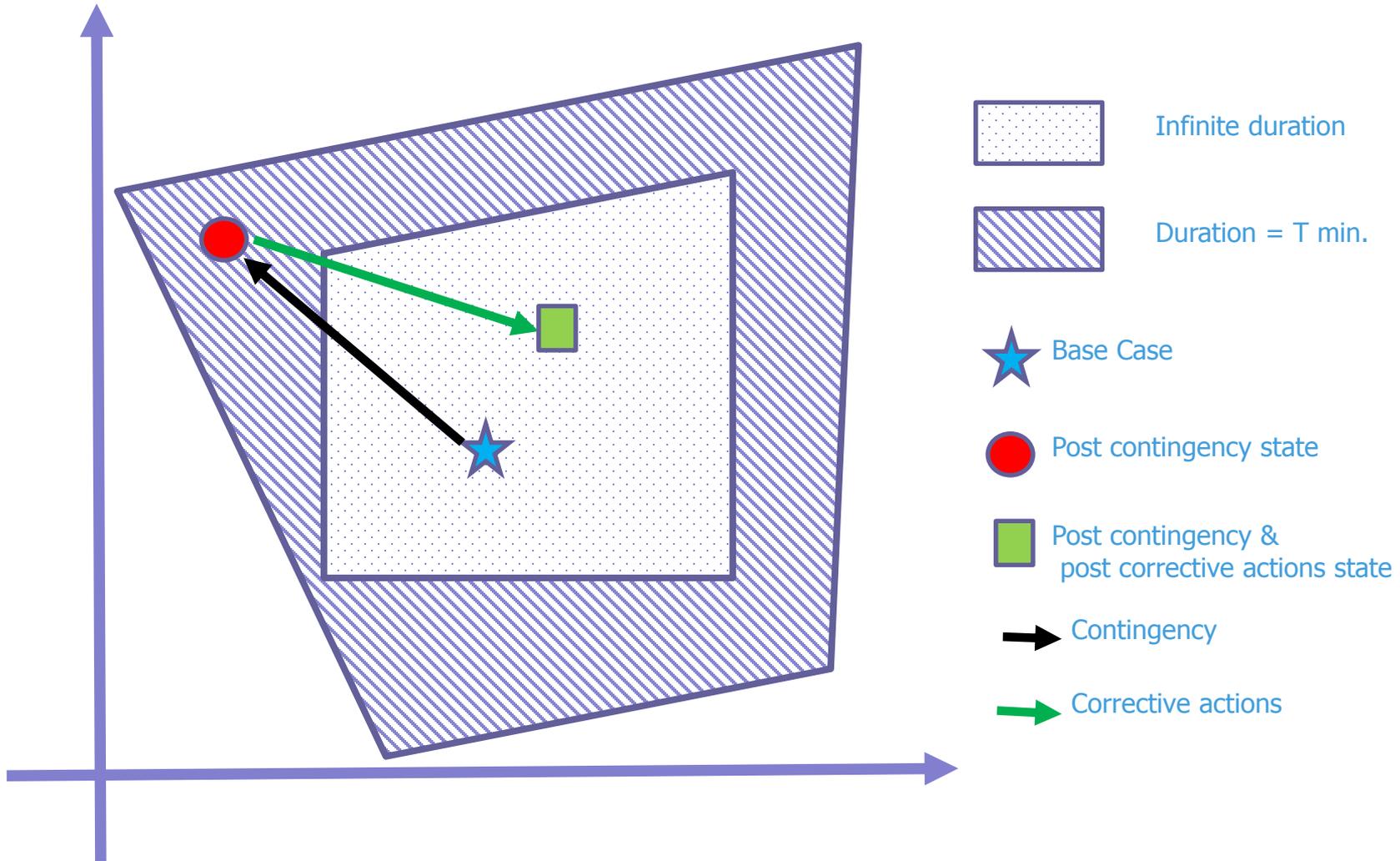


$t_p$ : Last time to decide preventive actions for time  $t$

$t_c$ : Post contingency

$t_{ca}$ : Post contingency & corrective actions

# Sequence of feasible domains (Illustration)



# Abstract formulation of SC-ACOPF

$$\min_{u_p} J(x, u_p) \quad u_p : \text{preventive actions}$$

$$\begin{cases} F(x, u_p) = 0 \\ G(x, u_p) \leq 0 \end{cases} \rightarrow \text{Base case}$$

$k \in \text{Set of contingencies}$

$$\begin{cases} F_k(x_k, u_p) = 0 \\ G_k(x_k, u_p) \leq 0 \end{cases} \rightarrow \text{Post contingency state}$$

$$\begin{cases} F_k(x_k^c, u_p, u_k^c) = 0 \\ G_k(x_k^c, u_p, u_k^c) \leq 0 \\ C_k(x_k, x_k^c, u_p, u_k^c) = 0 \end{cases} \rightarrow \text{Post contingency \& corrective actions state}$$

$u^c : \text{simulated corrective actions}$

# Final Steady state of closed loop controls in Static OPTIMIZATION PROBLEMS

▶ **Modeling of the final steady state of closed loop controls for the two post contingency states, simulation ...**

▶ **The ones acting faster than 1 min. for the post contingency state: AVR and speed generator of synchronous generators, switching of capacitor banks, HVDC links controls, ....**

▶ **The ones which are slower than 1 min. and faster than 15 min. for post contingency & corrective actions state: AGC, controls of PSTs, OLTC, ....**

▶ **Controls (u) have limits → The final state is not unique**  
x (controlled variables) = set points or  $u = u_{\max}$  or  $u = u_{\min}$

# Some Modeling Issues

- ▶ Generator Capability Curve ("D curve") or more (P,Q,V) 3D domain
- ▶ Node-Breaker modeling of Bus merging/splitting
- ▶ Phase Shifting Transformers: impedance depends on tap position
- ▶ HVDC links: Reactive/voltage modeling (LCC  $\neq$  VSC)
- ▶ Capacitors/Reactors banks (large banks)
- ▶ SVC, STATCOM, variable Series Compensation ....
- ▶ Closed loop controls: AVR, Speed governor, AGC, ...
- ▶ "Automatic" corrective actions:
  - ✓ RAS, SPS or simple predefined rules implemented by operators
  - If {some condition} then {action} ...
- ▶ Modeling of Active Distribution Networks

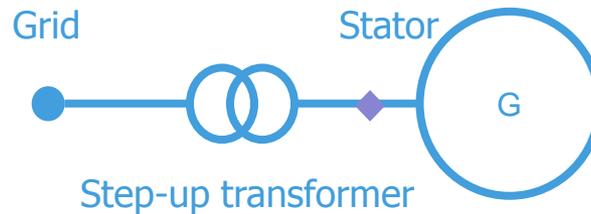
# Synchronous Generator (Pc , Vc )

## ► Generator Capability Curve ("D curve") or more (P,Q,V) 3D domain

✓ 3D convex domain: for a given P : (Q,V) domain, boundaries defined by a set of linear inequalities:

$$\alpha_l Q + \beta_l V \leq 1$$

✓ Which P,Q,V? Grid or stator side? What if step-up transf. is not explicitly represented



## ► AVR: Generalization of PV → PQ in Power flow

✓ Which voltage magnitude is controlled? Grid or Stator side?

✓  $V=V_c$  or (P,Q,V) is on one boundary of the domain, generally not  $Q=\text{constant}$

## ► Speed governor (primary power and frequency control)

✓ Generalization of "distributed slack bus" in Power flow: P active power

✓  $P = P_c + P_r N$ , N is scalar unique for one synchronous area but  $P_{\min} \leq P \leq P_{\max}$

# HVDC links

## ▶ Reactive/voltage behavior very different for LCC or VSC technology

✓ VSC is similar to a synchronous generator

✓ LCC, voltage magnitude and reactive are less controllable

➔ Complex modeling generally coordination with a OLTC

➔ which “reasonable” model for ACOPF?

Constant power factor  $Q = k \cdot P + Q_h$  due to harmonics filters with  $Q_h$  depending on  $P$

## ▶ Power flow control of HVDC link in // with AC power lines

✓  $P = P_c + K \cdot (\theta_1 - \theta_2)$  : Difference of voltage angles “emulation” of a AC line

## ▶ Reversal power flow for LCC

✓ Impossible to change rapidly the direction of the flows

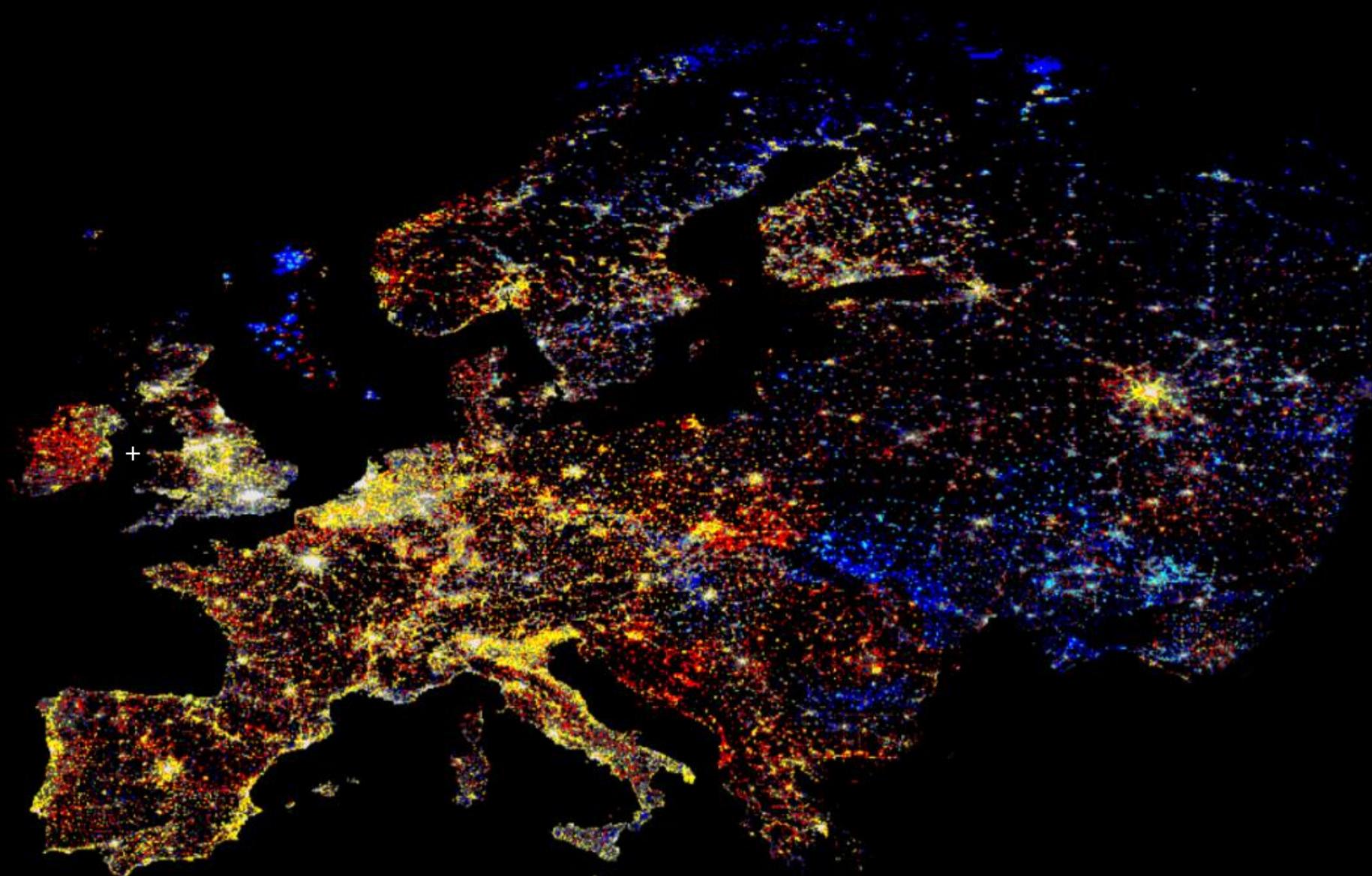
✓ More that 1 min. corrective actions .....

# Active Distribution Networks

- ▶ More and more dispersed generations (PV roof panel), Demand response programs, tomorrow storage
- ▶ The behavior seen from the transmission grid will not continue to look like even approximately to a constant P,Q load or anything like a ZIP model ....
- ▶ But it is impossible to have a detailed modelling of all the individual tiny “prosumers” in transmission grid decision making processes
- ▶ Decomposition of the total behavior between different types of fictitious aggregated components: a load, a wind farm, a PV farm and a storage device.
  - Each of them with a specific behavior in case of voltage magnitude variation and different participation to the system balancing

# Data Format & Data availability?

- ▶ The most common data formats don't support all these possible improvements.
- ▶ In the Griddata project led by U. of Michigan, we develop a new data format starting from a modeling document which propose improvements for most of these modeling issues.
- ▶ RTE can provide some realistic values for the required additional data and we are building step by step a collection of small size test cases with all the proposed improvements



THANK YOU FOR YOUR ATTENTION

[patrick.panciatici@rte-france.com](mailto:patrick.panciatici@rte-france.com)