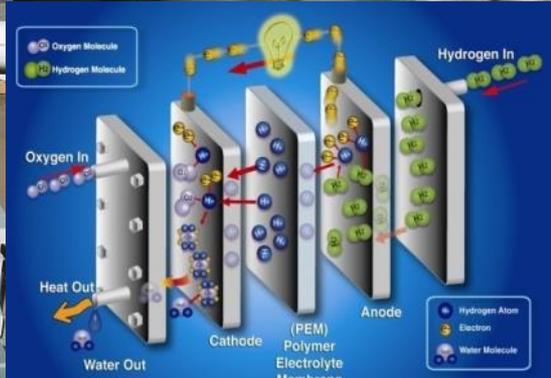


An overview of liquid hydrogen carrier R&D supported by the DOE Fuel Cell Technologies Office



ARPA-E Liquid Transportation Fuels Workshop
Denver, CO
August 27-28, 2015

Ned Stetson, PhD
U.S. Department of Energy
Fuel Cell Technologies Office
Hydrogen Storage Program Manager

- Definition of an ideal liquid hydrogen carrier
- How liquid hydrogen carriers could fit in the infrastructure
- Overview of key properties needed for an effective carrier
- Overview of DOE supported R&D on liquid carriers
 - Air Products and Chemicals Inc.
 - Hawaii Hydrogen Carriers
 - University of Oregon/Boston College
- H₂ Infrastructure – potential areas liquid carriers could offer advantages

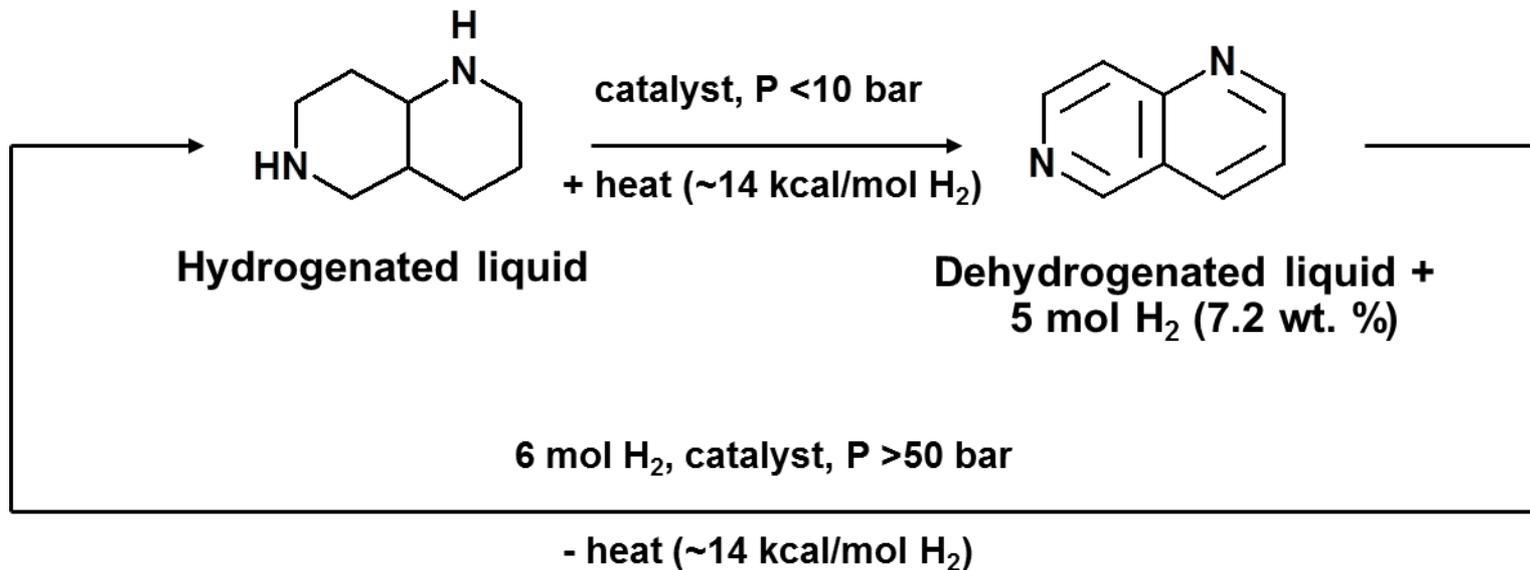
- Solid or gaseous carriers
- “One-way” carriers –
e.g., ammonia, hydrocarbon reformation
- Slurries – solid carrier suspended in a slurring agent –
e.g., ammonia borane or alane (AlH_3) in AR 20 silicon oil

- Stable with little to no release of hydrogen under the range of ambient conditions



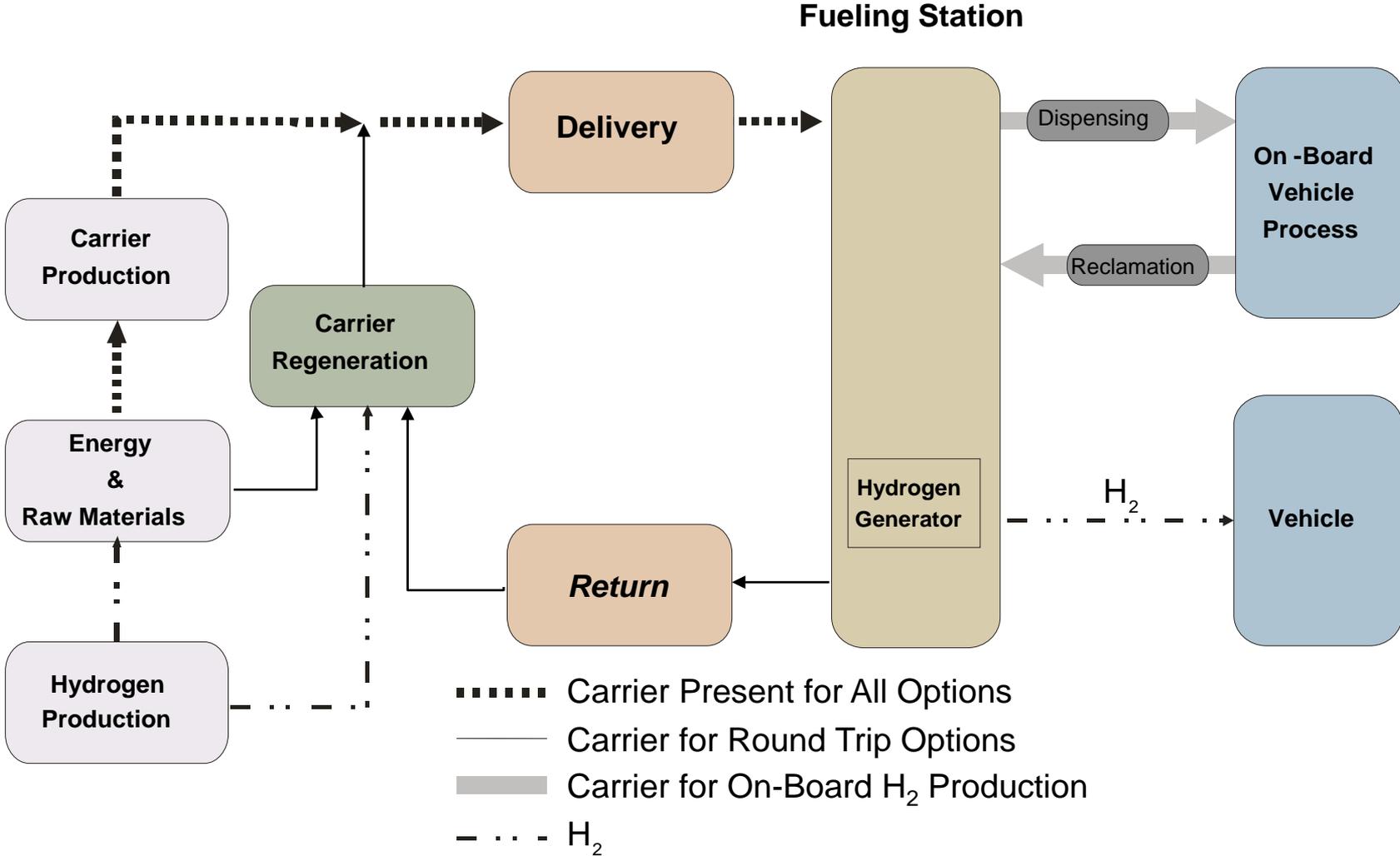
- Rapidly able to release hydrogen using available “waste” heat and temperature (e.g., PEM fuel cell)
- Remains in liquid phase throughout all stages of hydrogenation/dehydrogenation and temperature range
- Low volatility and able to be separated from the released hydrogen easily
- Little degradation on cycling (i.e., minimal side reactions and loss of volatile components) – long cycle life

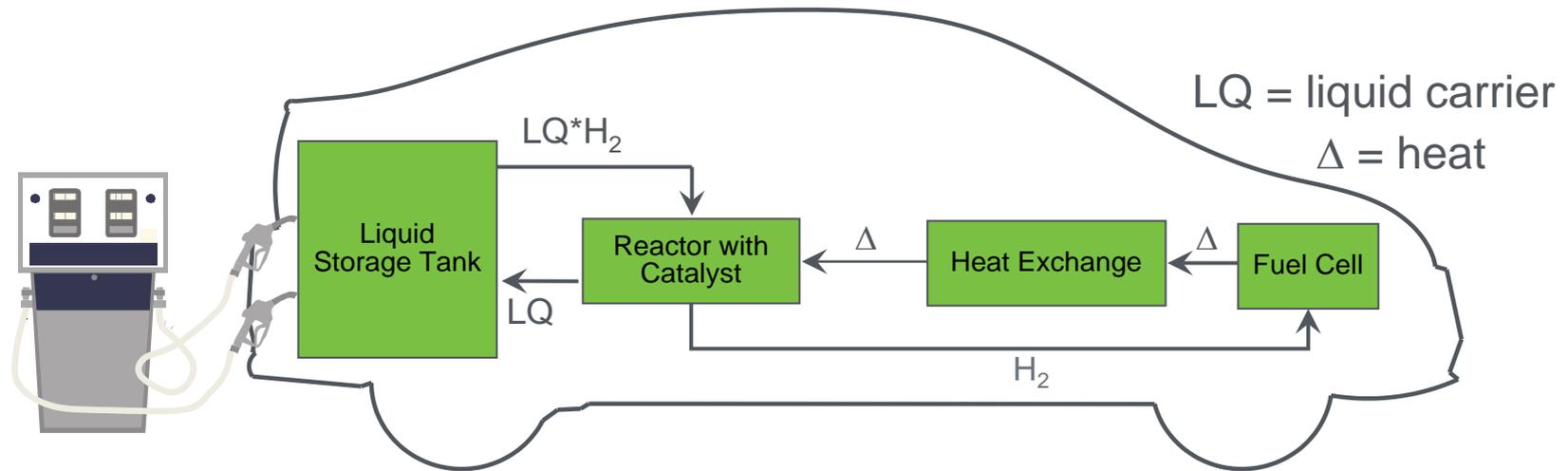
Operation scheme for “2-way” liquid hydrogen carriers



Estimate: ~72 liters of hydrogenated liquid carrier could reversibly store 5 kg of hydrogen at 7 wt.% and 1g/cc density

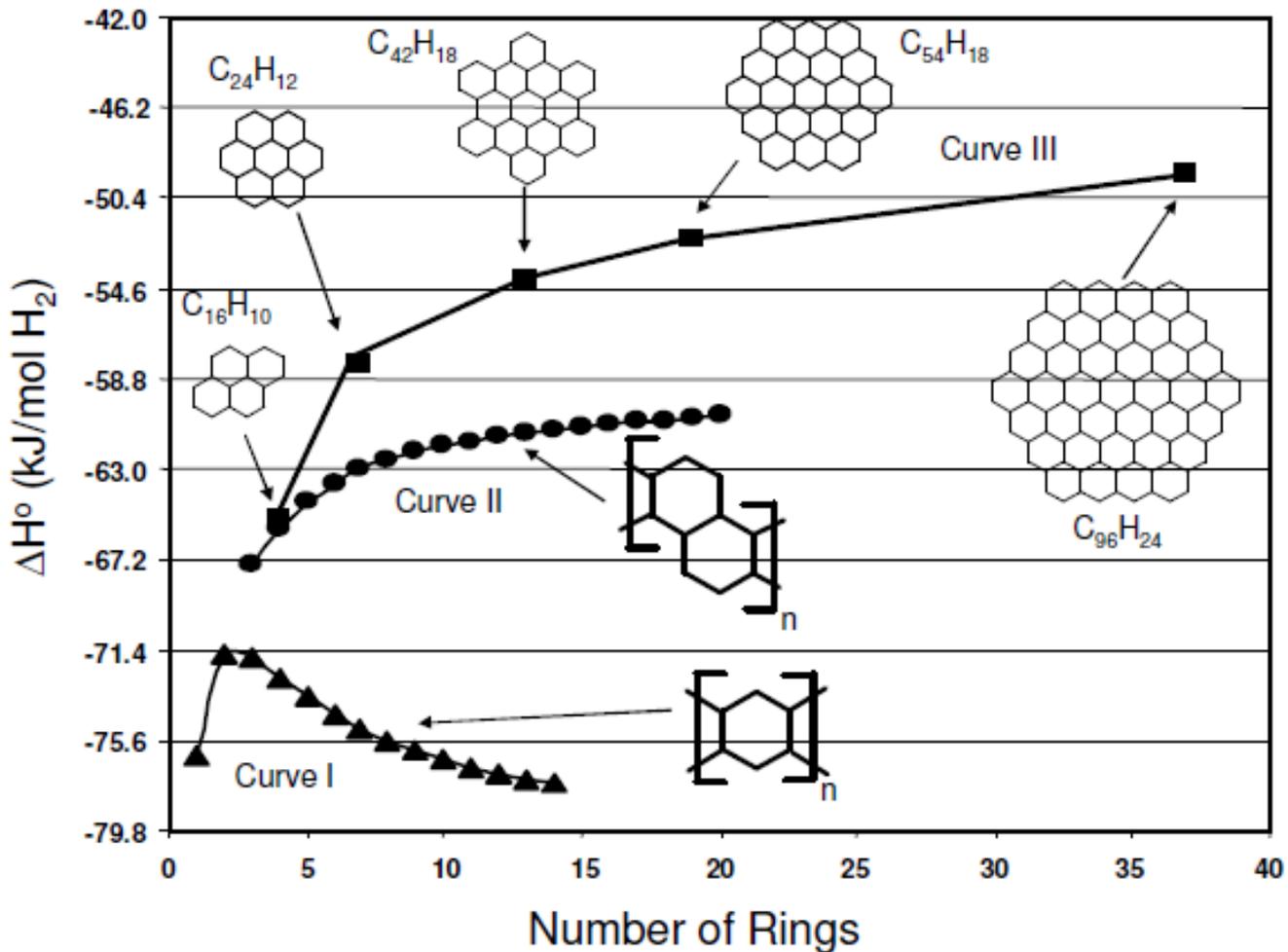
~ 50% of the volume required for 700 bar compressed H₂ at ambient temperatures!





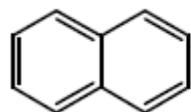
Currently not a focus area for the DOE-EERE Fuel Cell Technologies Office

Liquid Hydrogen Carrier Development

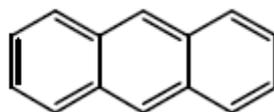


Calculated dehydrogenation enthalpy, H_D° (kJ/mole H_2), for three series of polyaromatic hydrocarbons as a function of the number of rings. The PM3 semi-empirical method was used for the calculations. (Air Products, Final Report, DOE Award # DE-FC36-04GO14006)

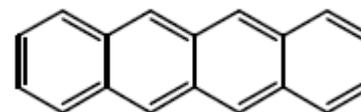
The aromatic stabilization energy of polyaromatic hydrocarbons is determined by the relative number of aromatic sextet structures in the molecules. (*Clar, E. in "Polycyclic Hydrocarbons", Academic Press, NY, 1964, Chapter 16*)



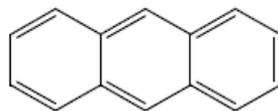
naphthalene



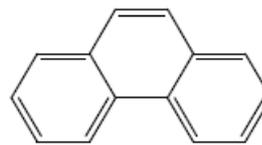
anthracene



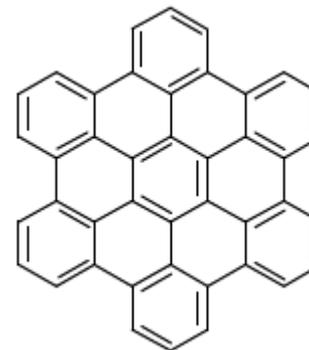
tetracene



anthracene

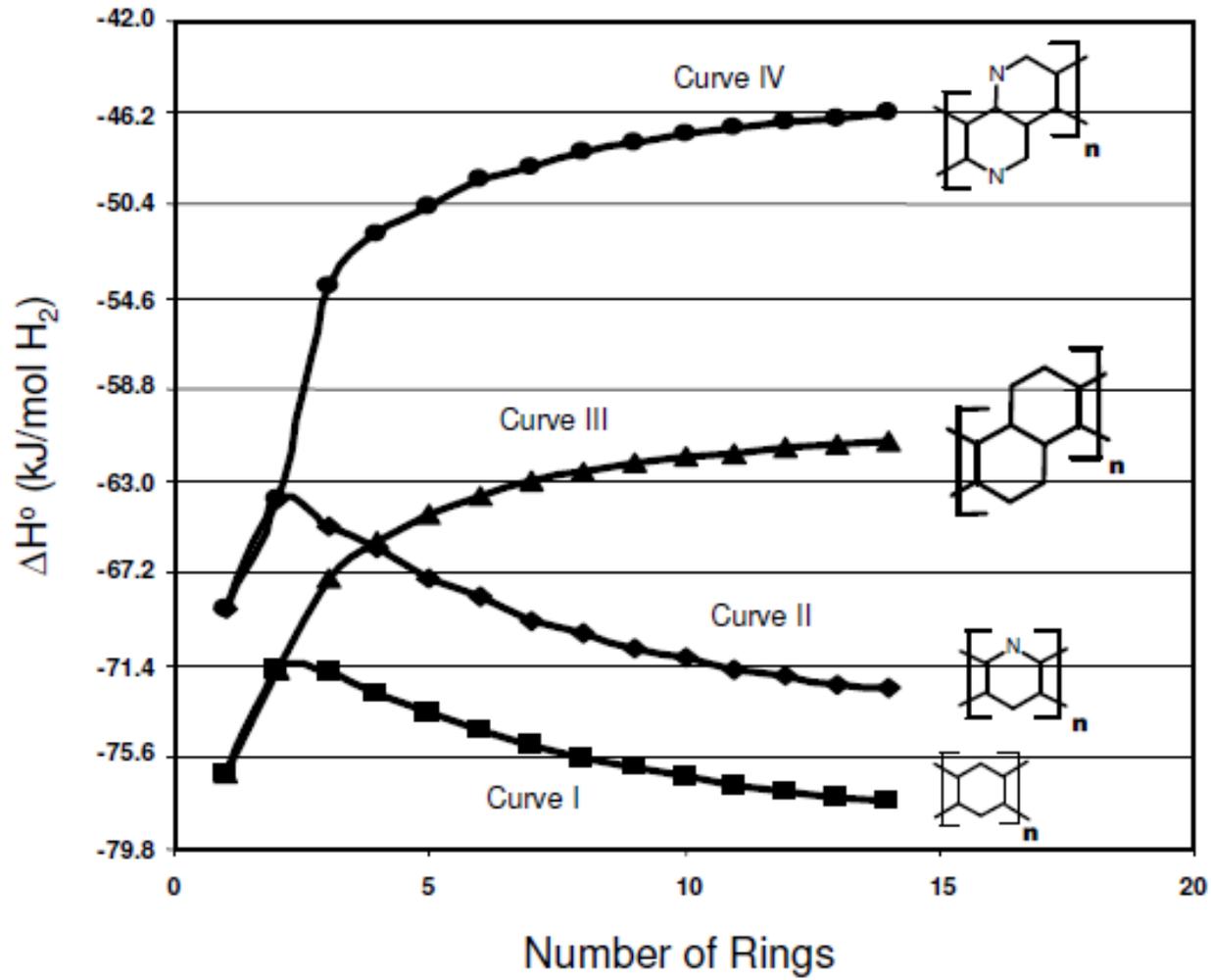


phenanthrene

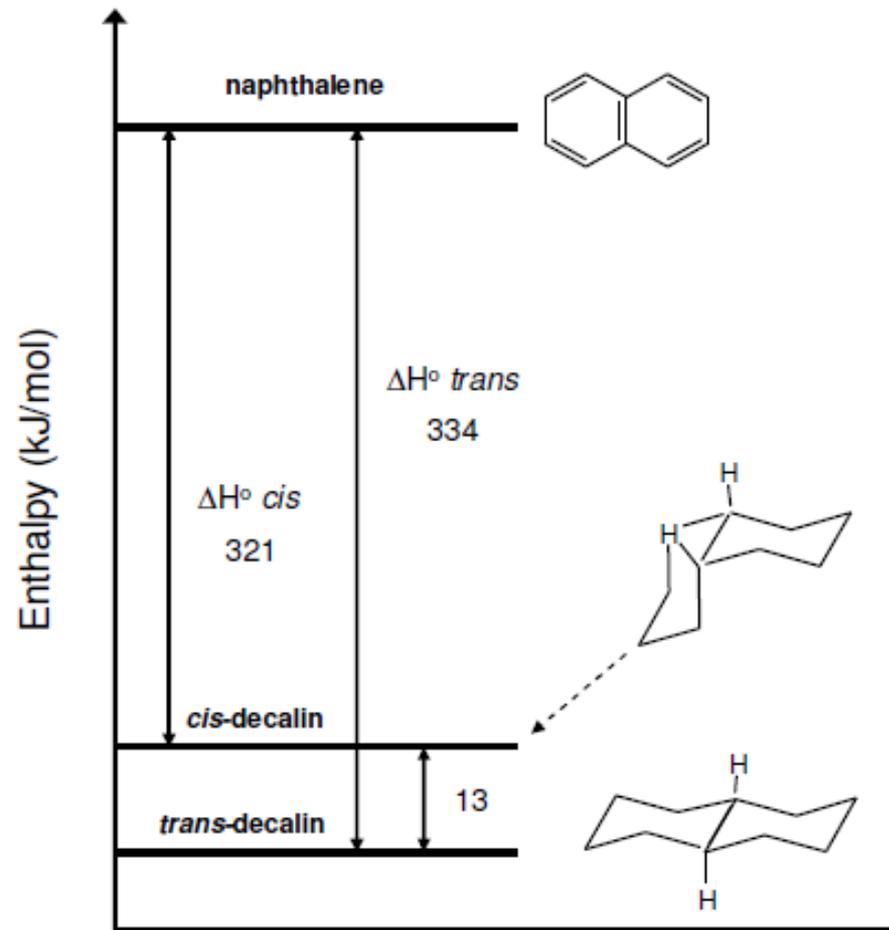


hexabenzocoronene

Effect of heteroatoms in the rings

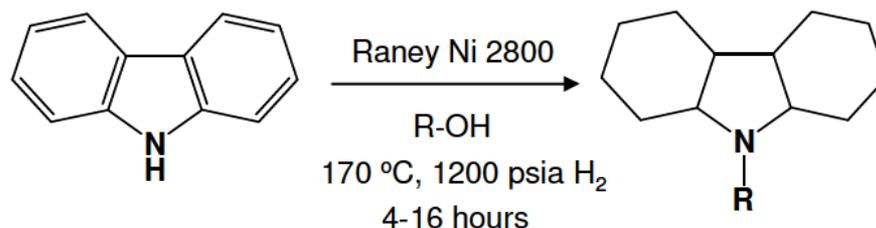


Calculated dehydrogenation enthalpy, H_D° (kJ/mole H_2) for N-heterocycles and the corresponding polyaromatic hydrocarbons (PM3 method) (*Air Products, Final Report, DOE Award # DE-FC36-04GO14006*)



Cis-trans isomerism in naphthalene and the relative energetics (Air Products, Final Report, DOE Award # DE-FC36-04GO14006)

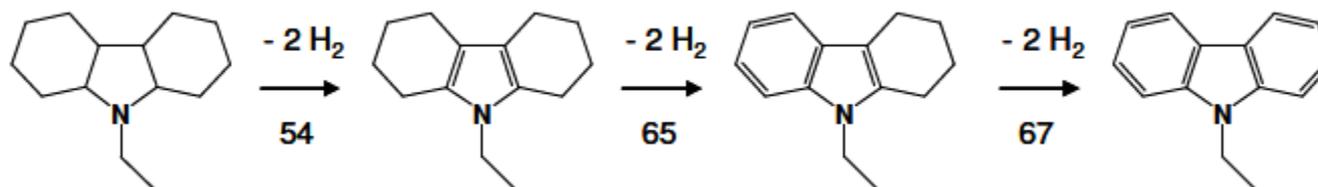
Molecule	Formula	Melting Point	Theoretical Capacity (wt.%)
Carbazole	$C_{12}H_9N$	250°C	6.7
N-methylcarbazole	$C_{12}H_9N-CH_3$	90°C	6.2
N-ethylcarbazole	$C_{12}H_9N-CH_2CH_3$	70°C	5.7



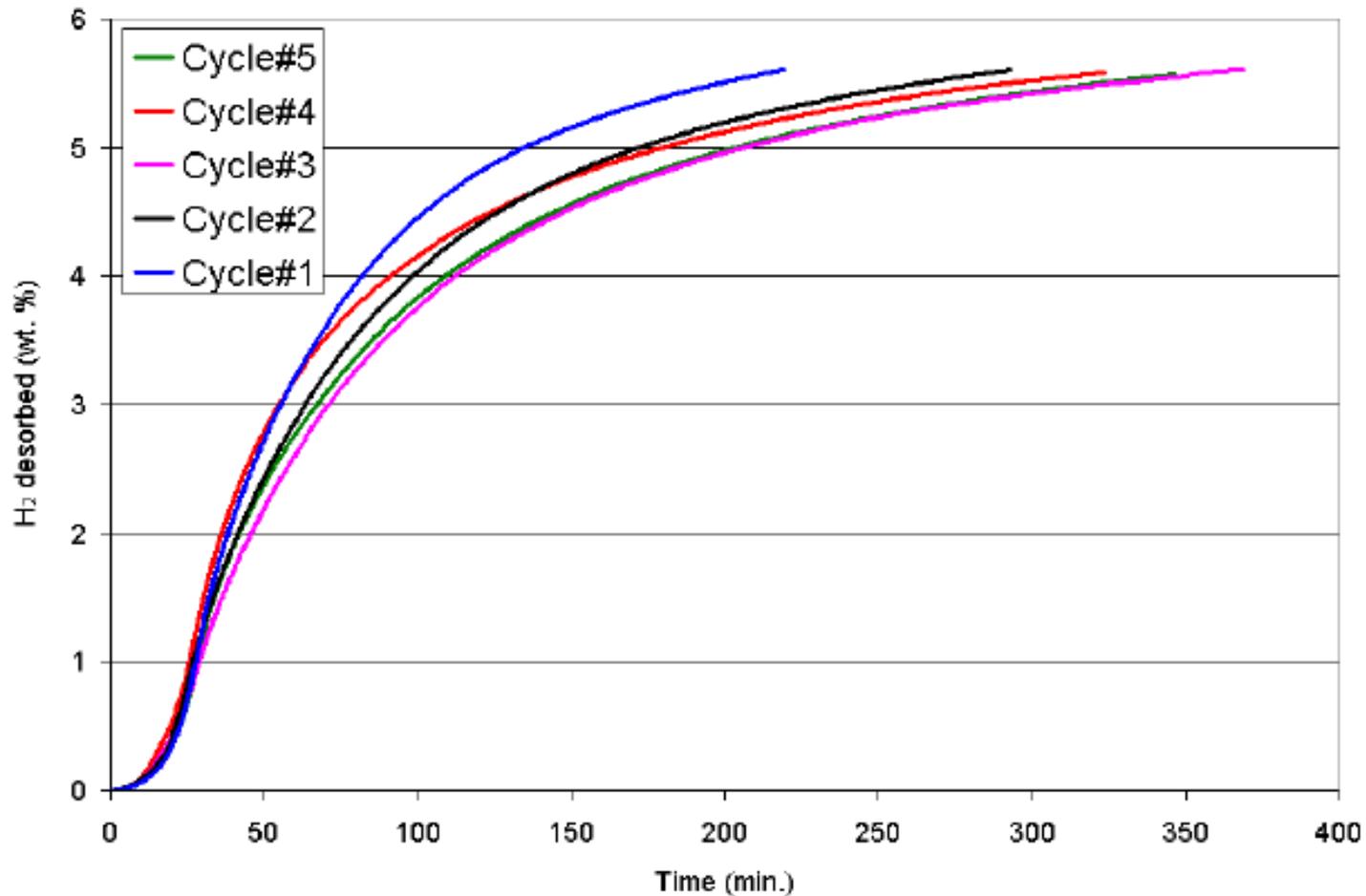
Yields of nickel-catalyzed hydrogenation and N-alkylation of carbazole.
(Air Products, Final Report, DOE Award # DE-FC36-04GO14006)

Alkyl group	Yield of perhydro-N-alkylcarbazole	Yield of partially hydrogenated N-alkylcarbazole	Hydrogenated carbazole
Methyl	98%	2%	0%
Ethyl	97%	3%	0%
n-propyl	97.5%	2.5%	0%
iso-propyl	59%	7%	34%

- Typical dehydrogenation experimental conditions for perhydro-N-alkylcarbazole performed by Air Products:
 - the dehydrogenation catalyst was slurried (1-5 wt.%) in liquid perhydro-N-alkylcarbazole
 - 1 atm. initial hydrogen pressure
 - temperature ramped at a controlled rate up to 150-200 °C
 - slurry stirred at 500-800 rpm
 - rate of hydrogen release from the reactor measured with a flow meter

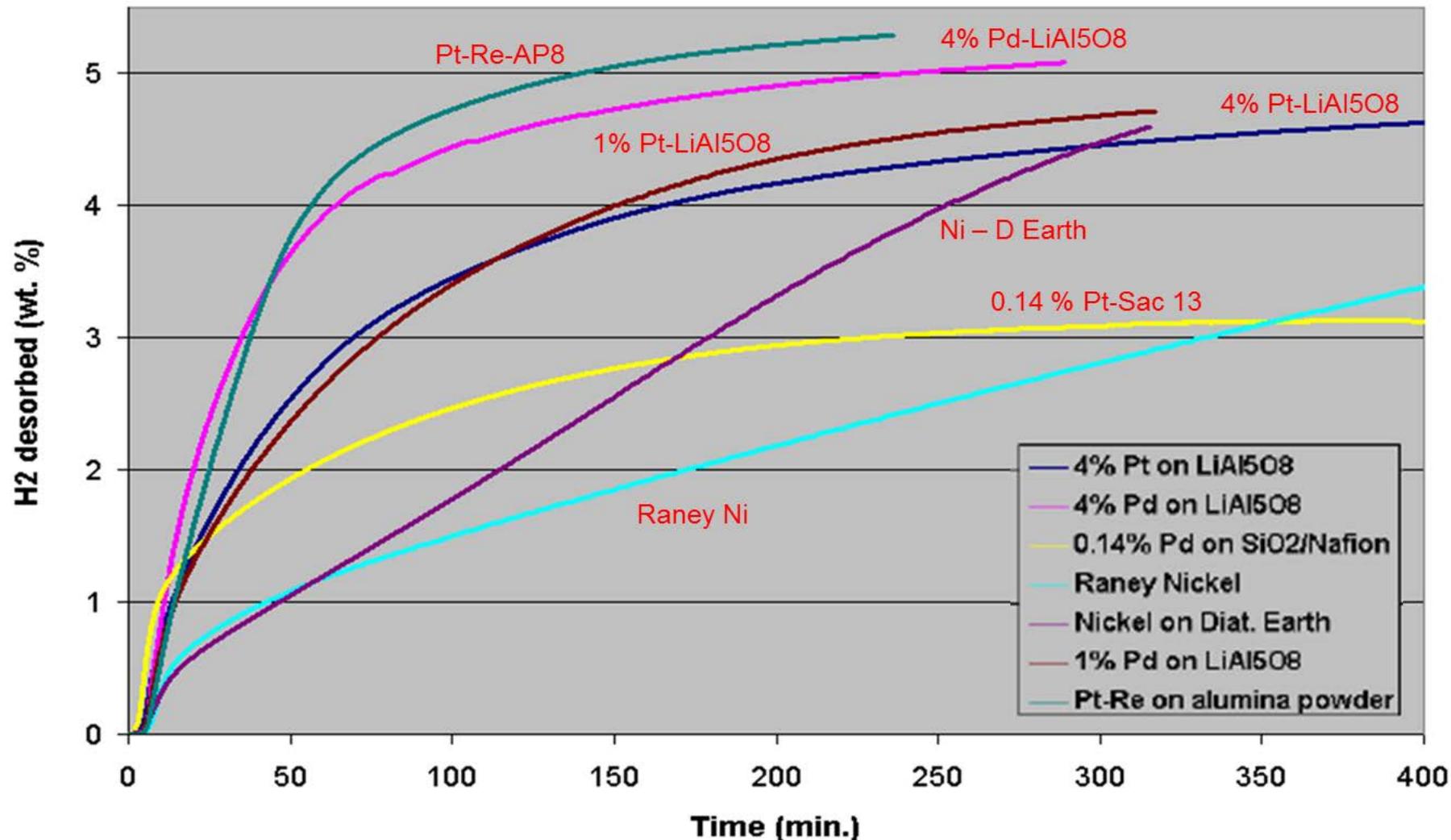


GC-MS analysis of intermediates indicate hydrogen released in steps of 2 hydrogen molecules. Scheme above includes calculated electronic energy change (DE; kJ/mol H₂) for the stepwise dehydrogenation of perhydro-N-ethylcarbazole



Five sequential dehydrogenation steps of hydrogenation/dehydrogenation cycling experiments of N-ethylcarbazole. (*Air Products, Final Report, DOE Award # DE-FC36-04GO14006*)

Effect of catalyst on dehydrogenation performance



Overlay of perhydro-N-ethylcarbazole hydrogenation data for a range of catalysts.
(Air Products, Final Report, DOE Award # DE-FC36-04GO14006)

Effect of catalyst, H₂ release rate and temperature on H₂ purity

Dehydrogenation of perhydro-N-ethylcarbazole with palladium/platinum on alumina. The table shows the temperature and hydrogen flow rate at the time when the samples were analyzed.

Pd on alumina

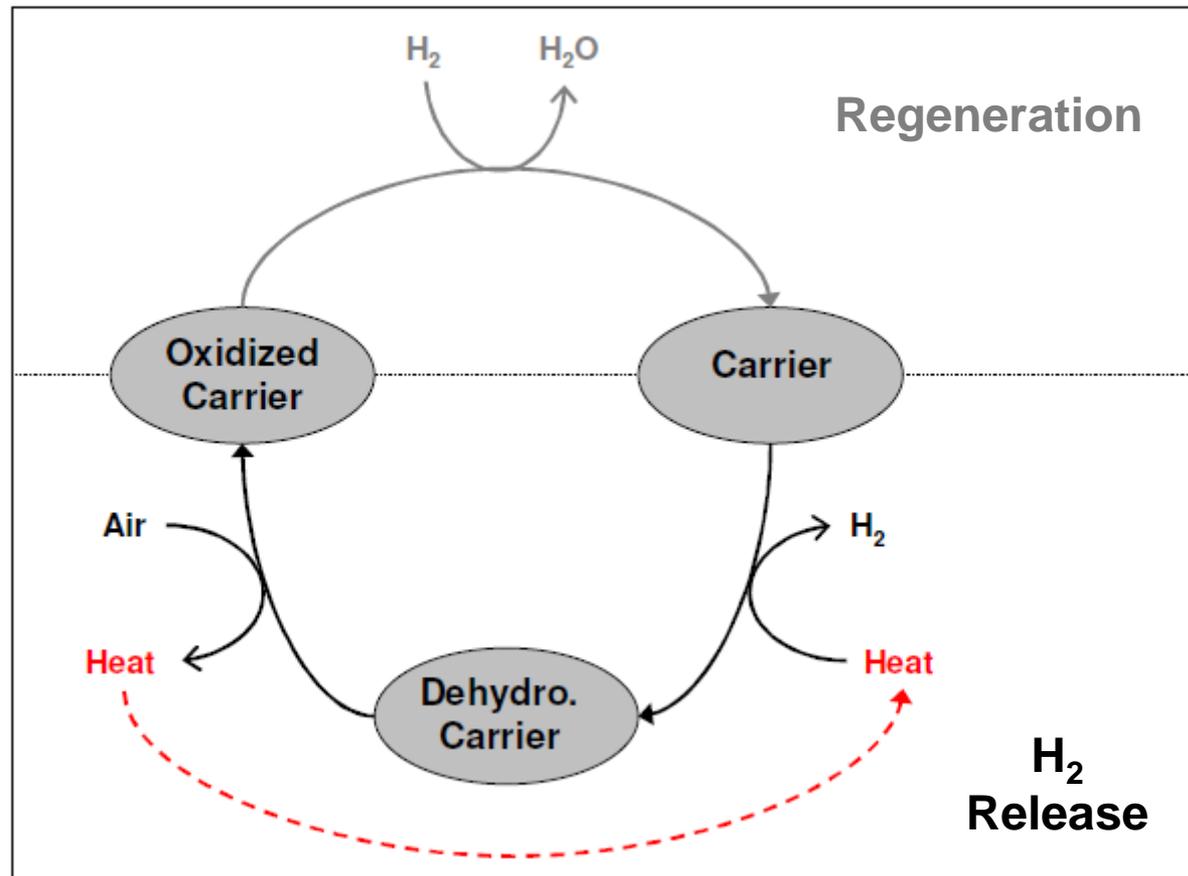
Temp (°C)	H ₂ Flow (sccm)	Methane Conc. (ppm)	Ethane Conc. (ppm)
144	5.0	177	2
147	6.4	164	10
149	7.3	137	19
152	8.1	99	31
154	9.0	80	34
197	45.0		1
197	39.0		13
197	35.0		23
197	30.0		23
197	26.0		25
197	5.0		44
197	4.6		47
197	4.4		48
197	4.1		47
197	3.9		48

Pt on alumina

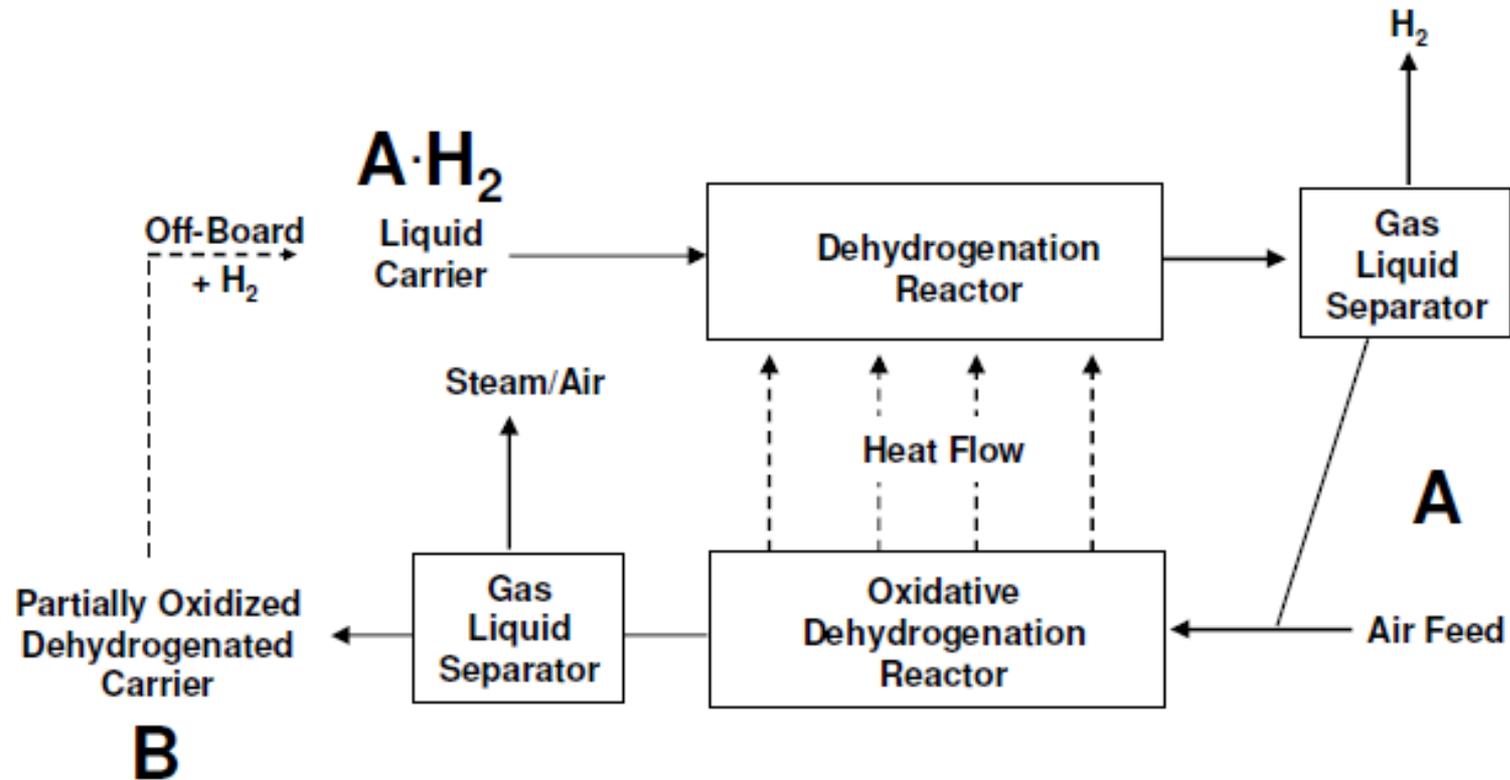
Temp (°C)	H ₂ Flow (sccm)	Methane Conc. (ppm)	Ethane Conc. (ppm)
144	5	196	44
147	6.4	194	163
153	7.3	188	374
155	8.1	178	631
157	9	169	991
197	58		2723
197	45		2865
197	32.9		3327
197	22.8		4146
197	17.5		5093
197	5		7244
197	4.8		7350
197	5.5		7398
197	4.9		7355
197	4		7343

How to supply the heat of enthalpy without consuming stored hydrogen?

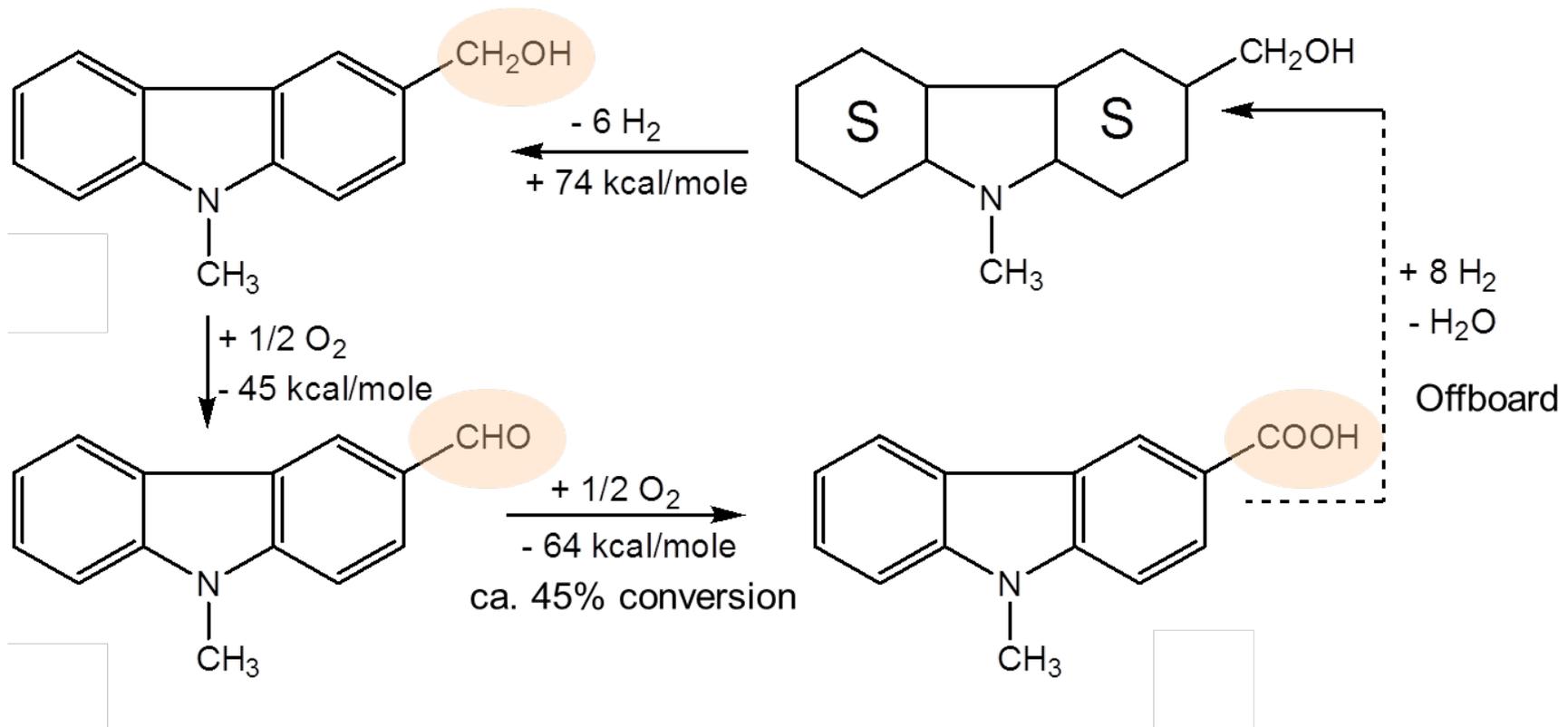
Potential solution – Development of an Autothermal concept



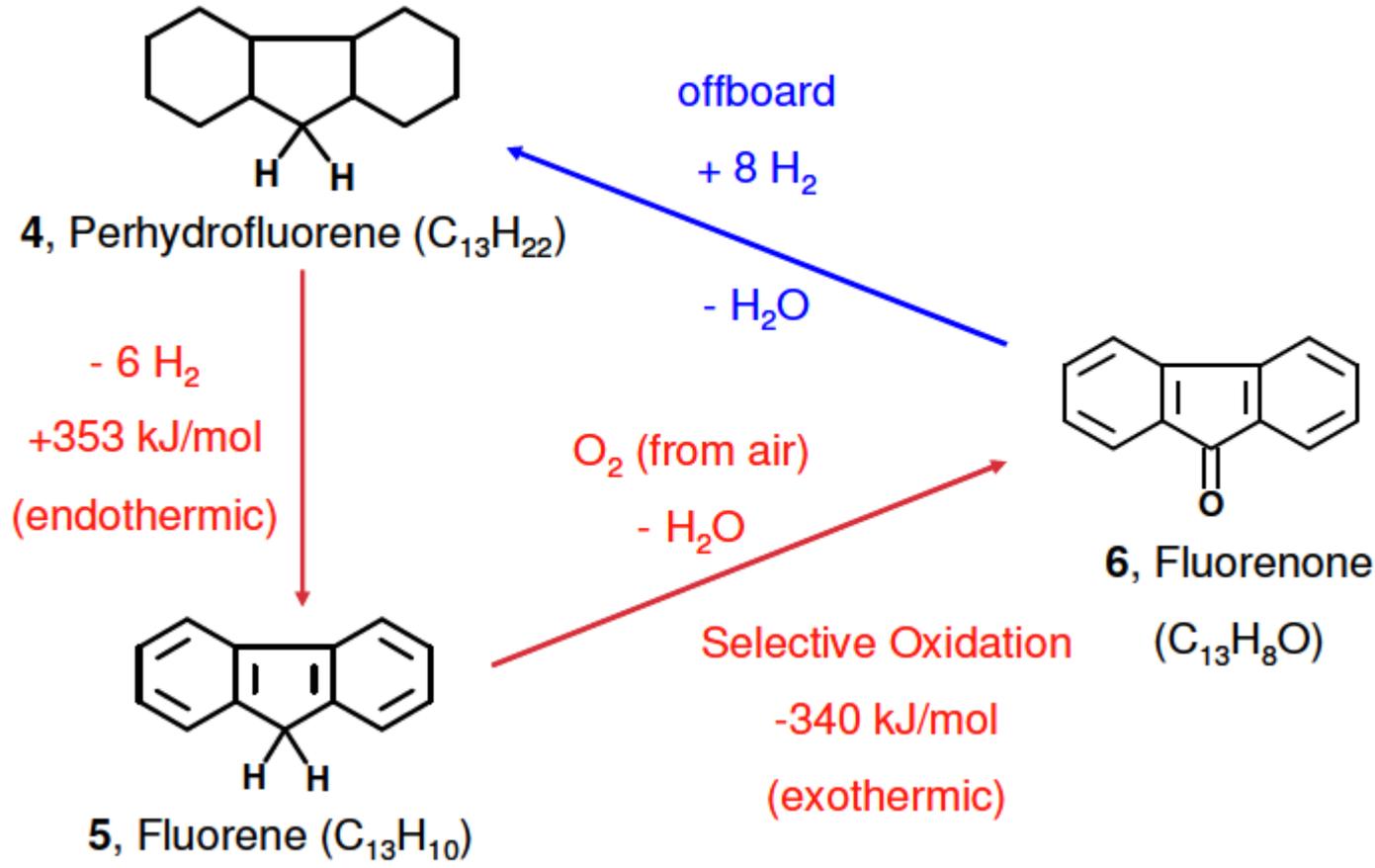
A general schematic of one autothermal carrier cycle



Autothermal dehydrogenation reactor system schematic.



- 5.4 wt.% H_2 (material basis) with no external input of heat
- Only partial conversion to the fully oxidized product is necessary for autothermal operation
- Highly selective catalytic chemistry is known for all of these steps



The perhydrofluorene/fluorene/fluorenone, dehydrogenation, selective oxidation and re-hydrogenation cycle.

For packed-bed reactor designs, two different reaction rate limitations were anticipated:

- 1) incomplete catalyst utilization caused by “drying out” of the catalyst surface, and
- 2) a reduction of the intrinsic reaction rate due to the effect of diffusion through the porous catalyst to the active metal sites, as measured by the effectiveness factor.

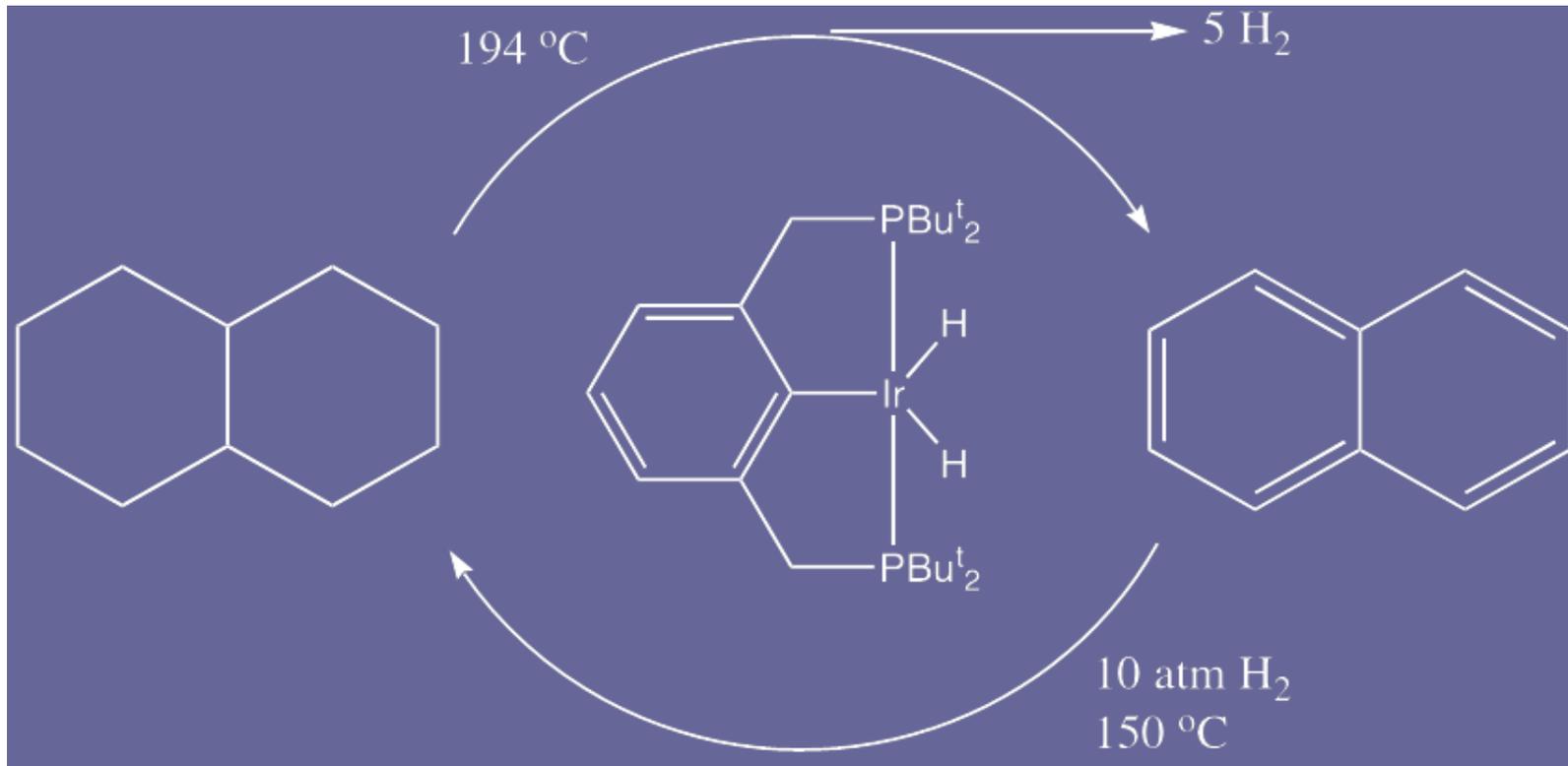
Alternative reactor designs investigated included:

- 1) Metal catalyst monoliths prepared from corrugated 0.05 mm iron/chromium foils coated with a tightly-adhering gamma alumina washcoat
- 2) Wicking microchannel reactor
- 3) Suspended slurry microchannel reactor – **considered the most promising**

H₂ liquid carrier economics are considered to be favorable, ***in the range of \$0.85 – \$4.50/kg H₂ delivery cost***, provided that certain targets can be achieved. Specific recommendations include:

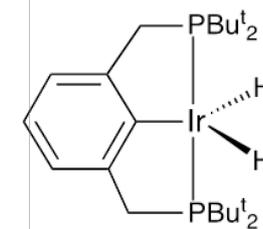
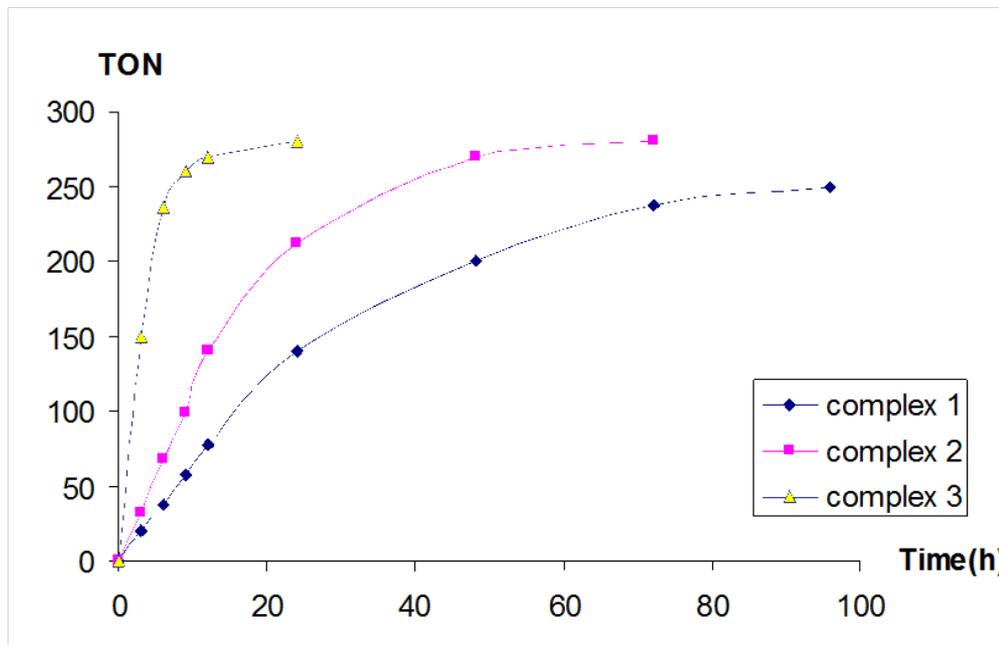
- reducing the liquid carrier cost to less than \$10/gallon,
- lowering the carrier melting point,
- meeting a catalyst productivity target of >1,000,000 kg LOHC processed per kg of catalytic metal,
- and reducing the carrier loss rate to <2% per year.

Homogeneous Catalyst Development

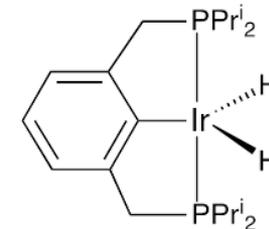


- First homogenous aliphatic dehydrogenation catalyst
- 3 orders of magnitude higher activity than heterogeneous catalyst temperatures as low $100 \text{ }^\circ\text{C}$
- Two-way catalyst

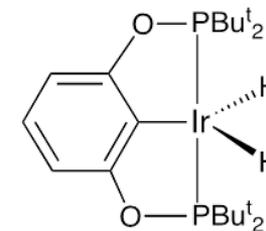
Hawaii Hydrogen Carriers presentation at the 2012 Hydrogen and Fuel Cells Technologies Annual Merit Review and Peer Evaluation Meeting, #ST-098, 17 May 2012



$\text{IrH}_2\{\text{C}_6\text{H}_3\text{-}2,6\text{-(CH}_2\text{P}^t\text{Bu}_2)_2\}$ (1)



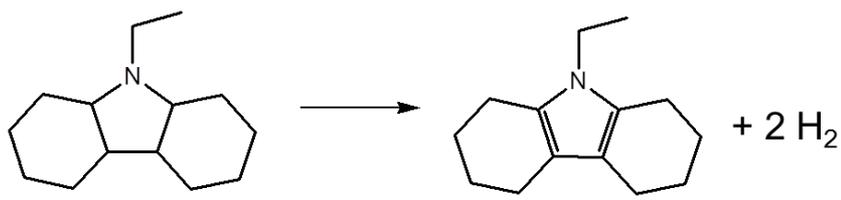
$\text{IrH}_2\{\text{C}_6\text{H}_3\text{-}2,6\text{-(CH}_2\text{P}^i\text{Pr}_2)_2\}$ (2)



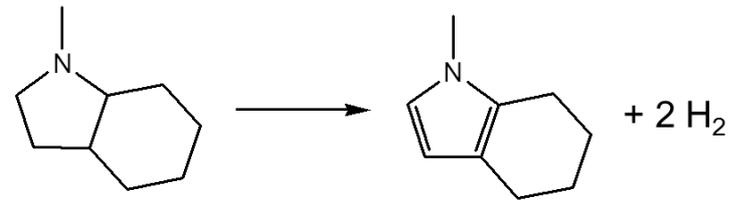
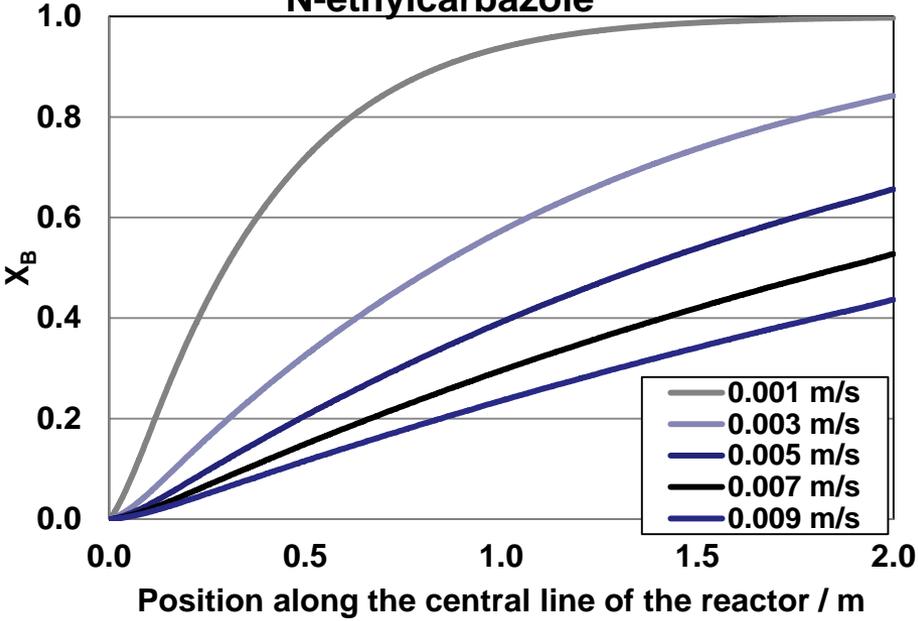
$\text{IrH}_2\{\text{C}_6\text{H}_3\text{-}2,6\text{-(OP}^t\text{Bu}_2)_2\}$ (3)

Dehydrogenation of N-ethylperhydrocarbazole using homogeneous Ir PCP pincer catalyst gives **higher rates of dehydrogenation at 2 orders of magnitude lower loadings than heterogeneous catalysts**

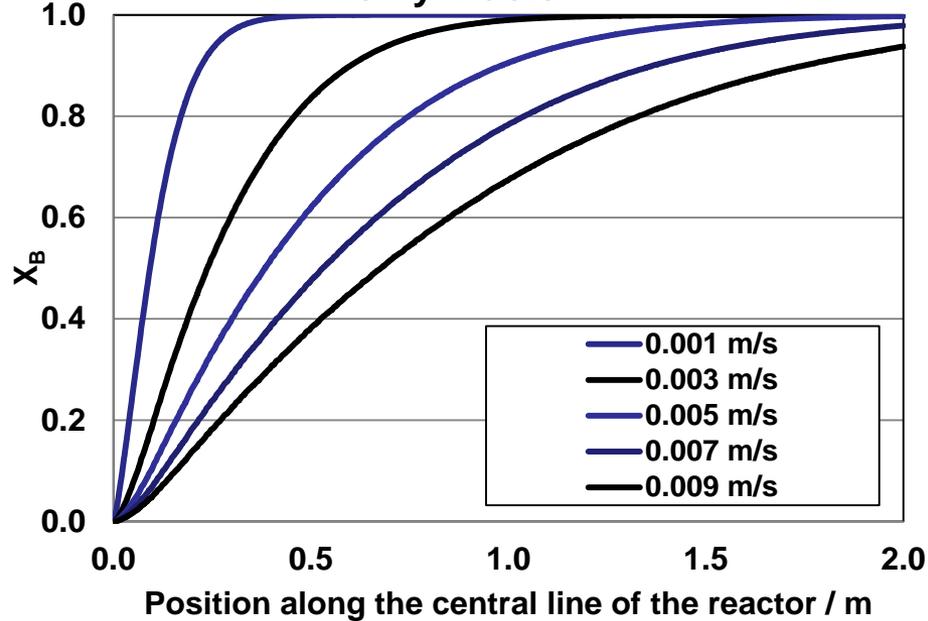
Alternative liquid carriers



N-ethylcarbazole



Methylindole

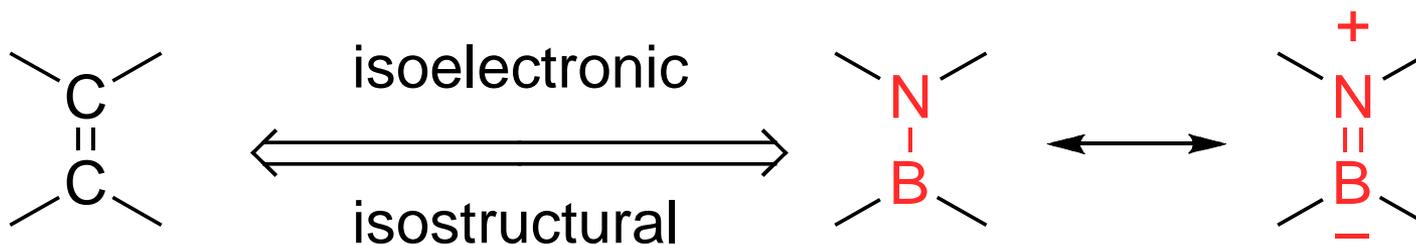


- Fixed reactor geometry and conditions
- Require near 100% conversion
- 5x improvement in H₂ production

MPHI gives higher throughput

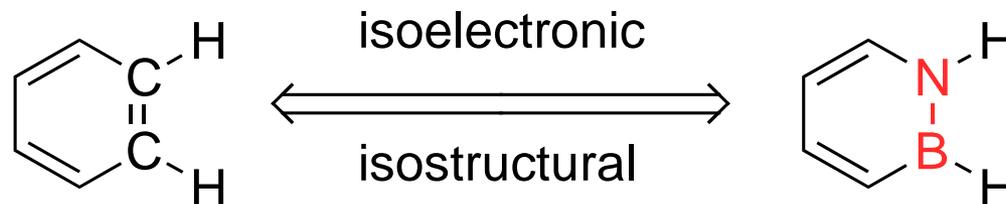
Hawaii Hydrogen Carriers presentation at the 2012 Hydrogen and Fuel Cells Technologies Annual Merit Review and Peer Evaluation Meeting, #ST-098, 17 May 2012

***Liquid Hydrogen Carrier
Development through
B-N substituted
heterocycles***



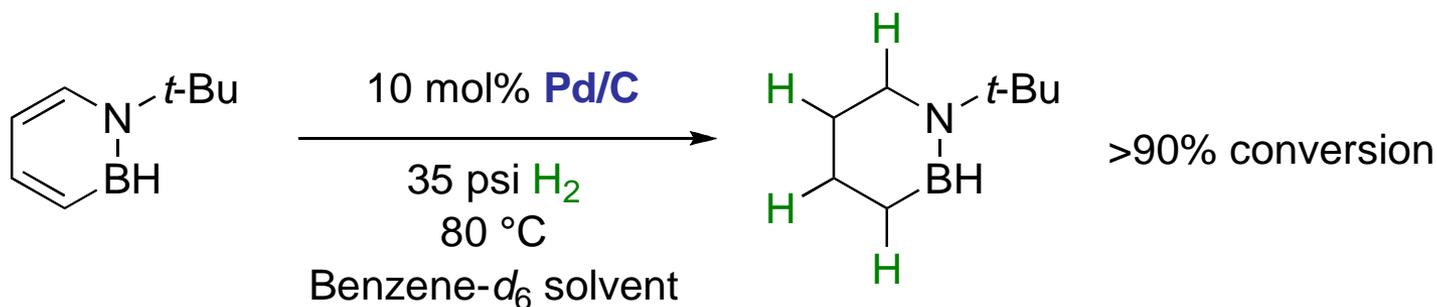
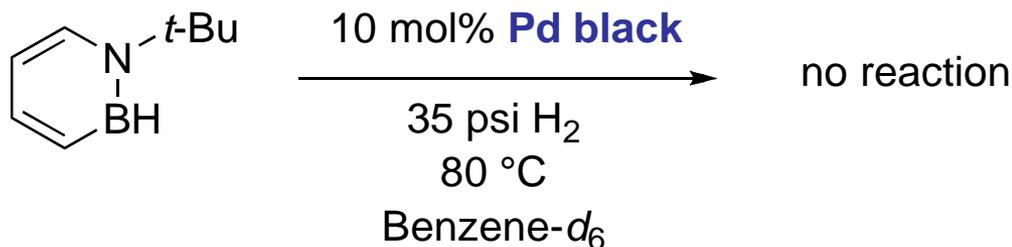
benzene

1,2-dihydro-
1,2-azaborine



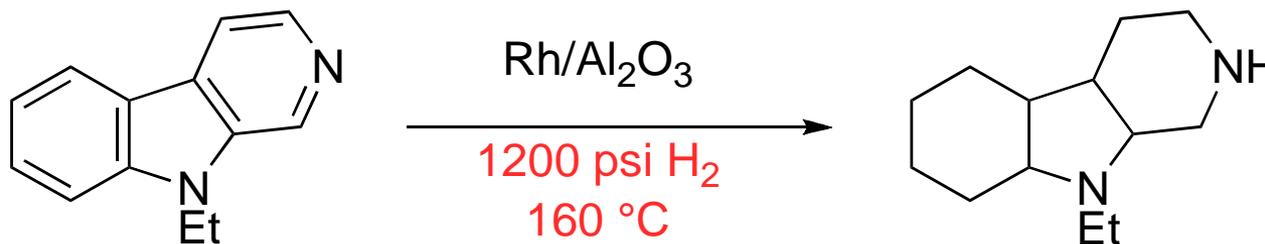
Research objectives:

- liquid-phase
- gravimetric density (> 6 wt. %)
- volumetric density (> 4.5 vol. %)
- favorable thermodynamics (H_2 absorption and desorption)
- efficient and easy regeneration (reversibility)
- Couple *exothermic* H_2 desorption from *BN* with *endothermic* H_2 desorption from *CC*



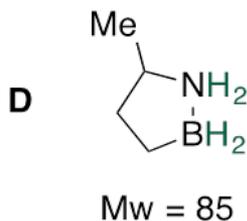
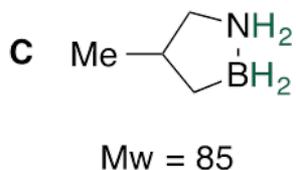
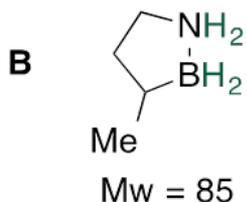
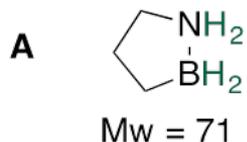
Benzene-d₆ is not hydrogenated!

VS.

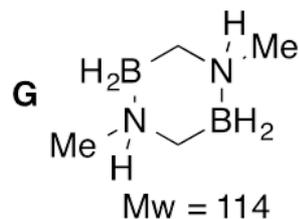
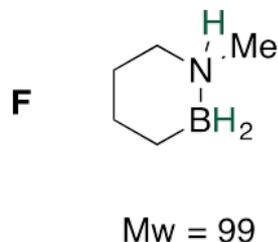
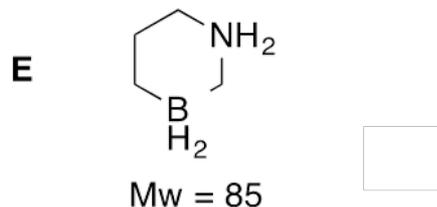


University of Oregon presentation at the 2009 Hydrogen and Fuel Cells Technologies Annual Merit Review and Peer Evaluation Meeting, #ST-016, 21 May 2009

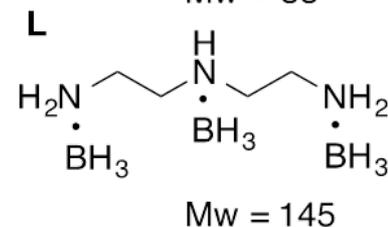
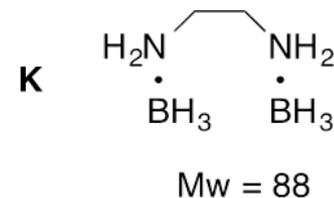
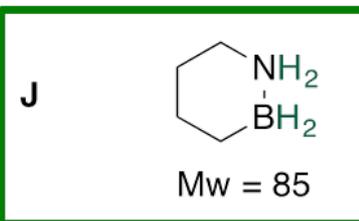
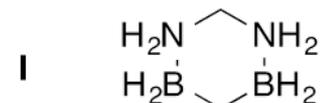
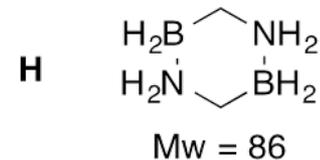
1) liquid phase

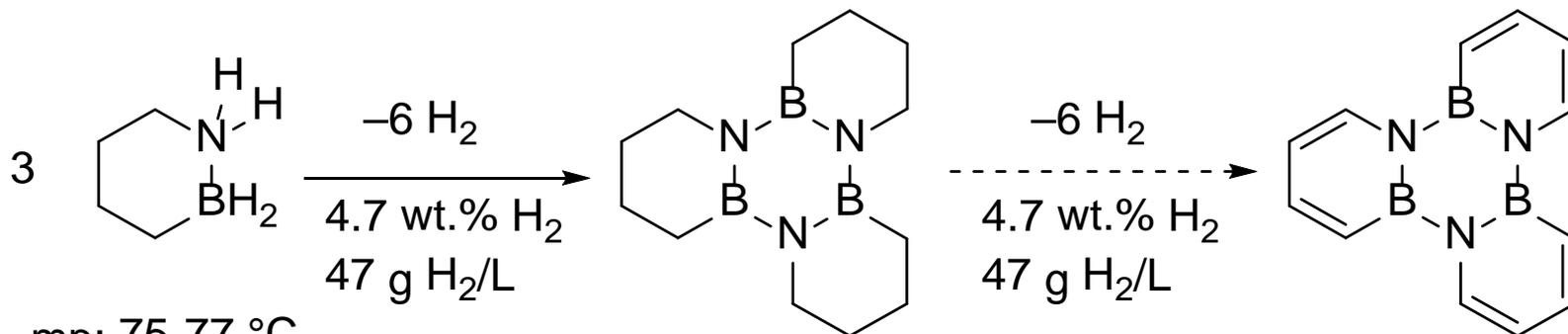


2) potentially reversible



3) high capacity





mp: 75-77 °C
d: 1.00 kg/L

Overall (-6 H₂)
 $\Delta H(\text{gas}) = -83.1$
 $\Delta H(\text{liquid}) = -59.6$
 $\Delta G(\text{gas}) = -107.3$

Per mol H₂:
 $\Delta G(\text{gas}) = -17.8$
 $\Delta H(\text{liquid}) = -10.0$
 $\Delta G(\text{THF}) = -13.6$

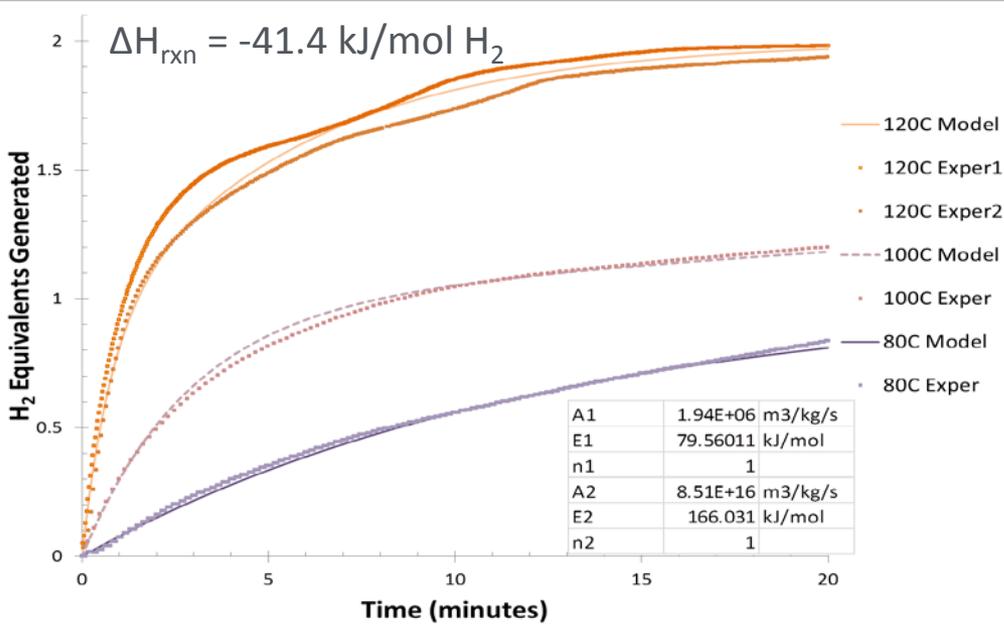
Overall (-6 H₂)
 $\Delta H(\text{gas}) = +102.3$
 $\Delta H(\text{liquid}) = +102.8$
 $\Delta DG(\text{gas}) = +49.4$

Energies in kcal/mol @ 298K
 Gas Phase: G3MP2
 Liquid Phase: G3MP2 (gas) +
 BP*0.025 (Trouton's rule)

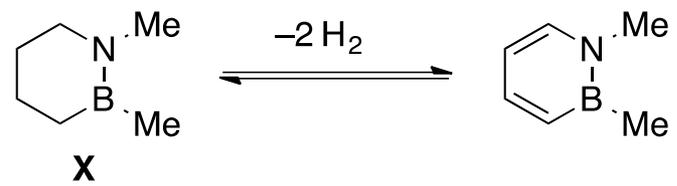
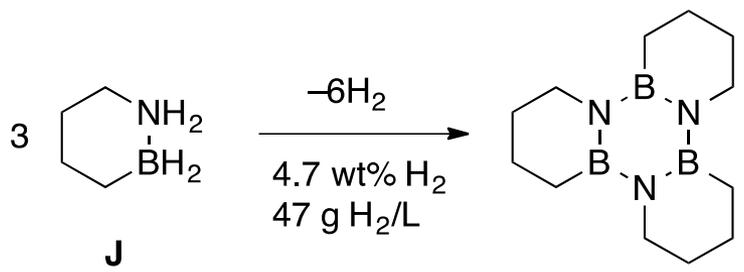
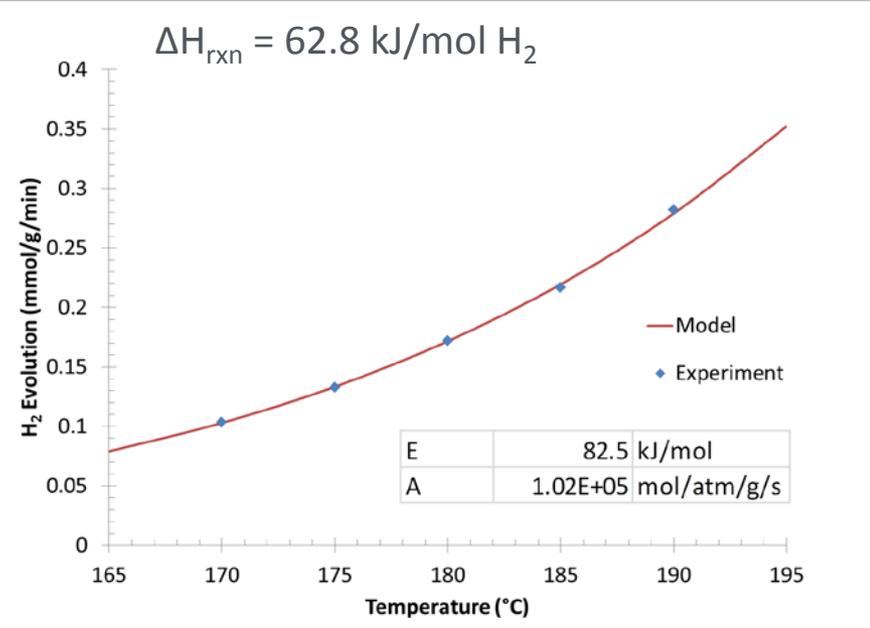
overall potential:
9.4 wt.%; 94 g H₂/L,
 potential **liquid phase**
 starting material at
 operating T

Per mol H₂:
 $\Delta G(\text{gas}) = -4.8$
 $\Delta H(\text{liquid}) = +4.0$
 $\Delta G(\text{THF}) = -3.6$

Exothermic Reaction



Endothermic Reaction



Thermodynamic Coupling Performed with Properties of Actual CBN Materials

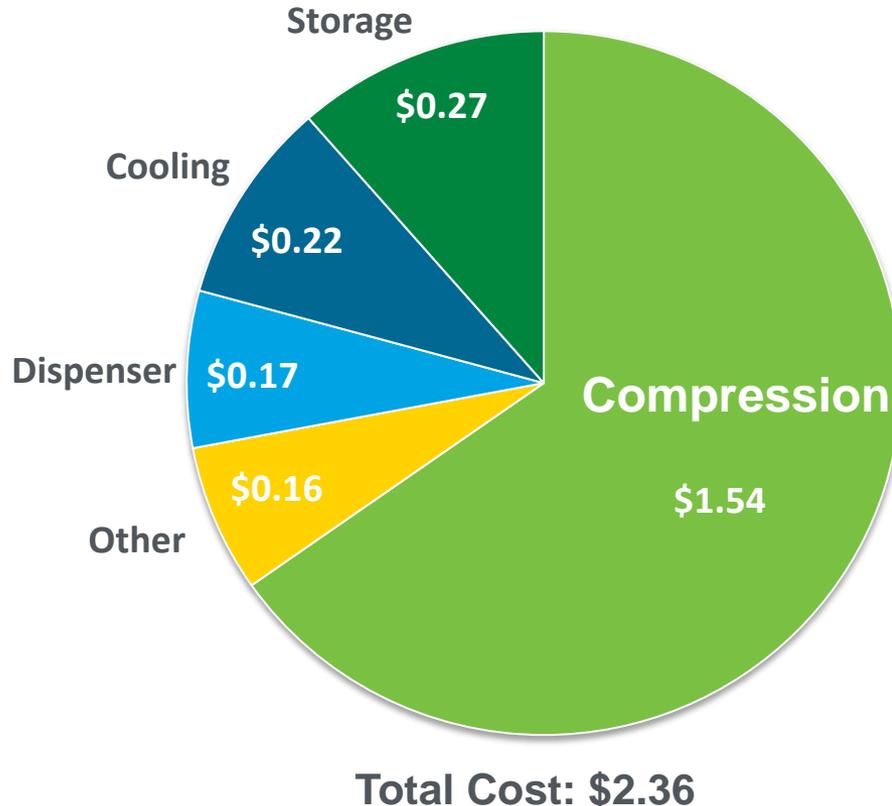
University of Oregon presentation at the 2015 Hydrogen and Fuel Cells Technologies Annual Merit Review and Peer Evaluation Meeting, #ST-104, 10 June 2015

H₂ Infrastructure considerations

Can liquid hydrogen carriers address key cost and performance issues of the hydrogen infrastructure?

- Transport/delivery
 - Capital cost of delivery equipment
 - Payload for delivery
- Forecourt
 - Storage
 - Compression

H₂ Compression, Storage and Dispensing (CSD) Cost Breakdown



- 2020 goal for H₂ cost at the pump is **<\$4/gge** (production and delivery cost included)
- **Compression** and **storage** are **75%** of the cost of H₂ station dispensing costs.

*Based on the pipeline scenario

Compression is a key challenge for the cost of delivering and dispensing H₂

- Air Products' reports available through the DOE Office of Science and Technology Information (*www.osti.gov*)
 - **Design and Development of New Carbon-based Sorbent Systems for an Effective Containment of Hydrogen** - DOE Award No. DE-FC36-04GO14006
 - **Reversible Liquid Carriers for an Integrated Production, Storage and Delivery of Hydrogen** - DOE Award Number DE-FC36-05GO15015
- FCTO Annual Progress Reports:
<http://energy.gov/eere/fuelcells/annual-progress-reports>
- FCTO Annual Merit Review Proceedings:
<http://energy.gov/eere/fuelcells/annual-merit-review-proceedings>

Thank you!